

# E&M Test 2 April 4<sup>th</sup> 2022

201300164 & 201300183 Fields and electromagnetism

**Instructions** You have **2 hours** to complete the test. Clearly indicate your name and student number on every sheet that you hand in. You may use a hand-written formula sheet containing maximum 10 equations. <u>This sheet must be handed in together with your answers.</u>

Before answering the questions, read all of them and start with the one you find easiest.

The amount of points to be obtained with each question is indicated next to the question number.

<u>Problem 1 (20pts/100)</u> A long and straight cylindrical hollow copper pipe with a very thick wall carries a current *I* along its positive axial *z*-direction. The current is distributed uniformly over the crosssection of the wall of the pipe. The inner radius of the pipe is R, the outer radius 2R.

- 1.a.) What is the direction of the B-field generated by this pipe?
- 1.b.) What is the direction of the corresponding vector potential A?
- **1.c.)** Calculate and sketch a graph of the magnitude of B versus the radial distance s to the axis of the pipe. Make sure to include all regions of space (s < R; R < s < 2R; and 2R < s) and indicate which component of B you are sketching.

**Problem 2 (15pts/100)** Consider a short cylindrical coil that carries a current  $l_f$  (figure 1.a).





Figure 1. a) short solenoid and b) the same solenoid partially loaded with a paramagnetic cylinder.

**2.a.)** Take the z-axis as the center axis of the coil. Sketch the field-lines of the magnetic induction **B** in the yz plane. Pay attention to both the shape and the direction of the field-lines.

Now a coaxial cylindrical paramagnetic rod ( $\chi_m > 0$ ) is <u>partially</u> entered in the coil (figure 1.b).

- **2.b.**) Copy figure (b) and sketch the bound surface currents  $K_B$  associated with the rod.
- **2.c.)** Add to your sketch in (b) the Lorentz force  $\mathbf{F}_{L}$  that acts on these surface currents just above the top of the coil. Clearly indicate the direction of this force. Is the rod attracted or expelled by the coil?

<u>Problem 3 (20pts/100)</u> Below you find 8 statements. For each of them, indicate whether the statement is 'true' (T) or 'not true' (NT). Also include a brief argument why you agree or not (minimum 1 & maximum 5 lines per statement). Read the statements carefully, each word may be important!

- **3.a.** Picture a carthesian xy-plane that carries a uniform surface current  $K_0$  in the x-direction. Parallel to this xy-plane, an infinitely long straight wire is suspended at a positive height z above the xy-plane. The wire carries a current  $I_0$  at an angle  $\alpha$  with the x-direction. This wire experience a downwards Lorentz force that is proportional to 1/z and proportional to  $\cos(\alpha)$ .
- **3.b.** If the current density **J** in a given region of space is uniform, the curl of the magnetic induction **B** generated by that current must be zero.

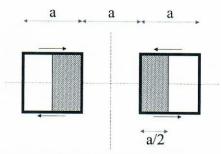
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- 3.c. When we double the current in a solenoidal coil that is filled with a linear magnetic material, the energy associated with the magnetic field inside that material quadruples.
- 3.d. Two wires carry identical but opposite currents. Any closed path-integral of the magnetic induction B along a path that encloses just these two currents must be zero, regardles of the orientation of the wires with respect to each other.
- **3.e.** When we move a lump of material with magnetization **M** along the axis of an infinitely long straigth solenoid, it depends on the direction of the motion whether this costs or releases energy.
- 3.f. The direction of the bound volumetric current density  $J_B$  inside a material with non-uniform magnetization M is always perpendicular to M.
- 3.g. The free current density J inside a conductor always follows the electric field lines E.
- 3.h. The self-induction L of a coil is proportional to the current that flows in the coil.

<u>Problem 4 (25pts/100)</u> Figure 2 schematically shows the cross section of a thick toroidal coil with a square cross-section. The thick black lines represent the outside of the coil and the black arrows next to the square cross-section indicate the direction of the current / that flows through the coil.

There are N turns in total in this coil. The inner diameter of the coil is a, the outer diameter is 3a. A material with a relative magnetic susceptibility  $\mu_r$ =2 occupies the inner half of the inside of the coil (grey parts).

- **4.a)** Derive an expression for the magnetic field **H** (magnitude and direction) as a function of the radial distance *s* to the vertical center line; and sketch a graph of the magnitude of the relevant component of **H** as a function of *s*.
- **4.b)** Derive an expression for the magnetic induction  $\bf B$  as a function of s and sketch the relevant component of  $\bf B$  in the graph that you created for part 4.a.
- **4.c)** Derive an expression for the magnetization M and from this, derive expressions for the surface current density  $K_B$  and the volume current density  $J_B$ . Explain the direction of these currents with respect to the current in the coil.



**Figure 2:** Toroidal coil partially filled with a magnetizable material (problem 4).

<u>Problem 5 (20pts/100)</u> Two concentric circular wire loops lie in the same (xy) plane. They are constructed from the same type of round wire with diameter d and electrical resistivity  $\rho$ . The radius of the inner loop is  $R_1$ , that of the outer loop  $R_2 >> R_1$ .

- **5.a.)** A current  $I_2$  runs in the  $+\phi$  direction in the outer loop. Show that the magnetic induction  $\mathbf{B}_2$  generated by this current in the center of the loops is  $\mathbf{B}_2 = \frac{\mu_0 I_2}{2R_2} \hat{\mathbf{z}}$ , with z the direction perpendicular to the plane of the circles.
- **5.b.)** Work out the approximate magnetic flux  $\phi_{12}$  through the inner loop due to this field  $B_2$ . Since  $R_1$  <<  $R_2$ , you may neglect the variation of  $B_2$  over the surface of the inner loop.
- **5.c.)** The current  $I_2$  is an alternating current:  $I_2(t) = I_0 \sin(\omega t)$ . What is the current  $I_1(t)$  induced in the inner loop by the alternating current in the outer loop?
- **5.d.)** The alternating current  $I_2$  is switched off and a constant current  $I_1$  is injected in the *inner* loop. What is the magnetic flux  $\phi_{21}$  through the *outer* loop that is generated by this current  $I_1$ ?

#### **FUNDAMENTAL CONSTANTS**

$$\epsilon_0 = 8.85 \times 10^{-12} \,\text{C}^2/\text{Nm}^2$$
 (permittivity of free space)

$$\mu_0 = 4\pi \times 10^{-7} \,\text{N/A}^2$$
 (permeability of free space)

$$c = 3.00 \times 10^8 \,\text{m/s} \qquad \text{(speed of light)}$$

$$e = 1.60 \times 10^{-19} \,\mathrm{C}$$
 (charge of the electron)

$$n = 9.11 \times 10^{-31} \,\text{kg}$$
 (mass of the electron)

# SPHERICAL AND CYLINDRICAL COORDINATES

### **Spherical**

$$\begin{cases} x = r \sin \theta \cos \phi \\ y = r \sin \theta \sin \phi \\ z = r \cos \theta \end{cases} \begin{cases} \hat{\mathbf{x}} = \sin \theta \cos \phi \, \hat{\mathbf{r}} + \cos \theta \cos \phi \, \hat{\boldsymbol{\theta}} - \sin \phi \, \hat{\boldsymbol{\phi}} \\ \hat{\mathbf{y}} = \sin \theta \sin \phi \, \hat{\mathbf{r}} + \cos \theta \sin \phi \, \hat{\boldsymbol{\theta}} + \cos \phi \, \hat{\boldsymbol{\phi}} \\ \hat{\mathbf{z}} = \cos \theta \, \hat{\mathbf{r}} - \sin \theta \, \hat{\boldsymbol{\theta}} \end{cases}$$

$$\begin{cases} r = \sqrt{x^2 + y^2 + z^2} \\ \theta = \tan^{-1}(\sqrt{x^2 + y^2}/z) \\ \phi = \tan^{-1}(y/x) \end{cases} \begin{cases} \hat{\mathbf{r}} = \sin \theta \cos \phi \, \hat{\mathbf{x}} + \sin \theta \sin \phi \, \hat{\mathbf{y}} + \cos \theta \, \hat{\mathbf{z}} \\ \hat{\boldsymbol{\theta}} = \cos \theta \cos \phi \, \hat{\mathbf{x}} + \cos \theta \sin \phi \, \hat{\mathbf{y}} - \sin \theta \, \hat{\mathbf{z}} \\ \hat{\boldsymbol{\phi}} = -\sin \phi \, \hat{\mathbf{x}} + \cos \phi \, \hat{\mathbf{y}} \end{cases}$$

### Cylindrical

$$\begin{cases} x = s\cos\phi \\ y = s\sin\phi \\ z = z \end{cases} \begin{cases} \hat{\mathbf{x}} = \cos\phi \hat{\mathbf{s}} - \sin\phi \hat{\boldsymbol{\phi}} \\ \hat{\mathbf{y}} = \sin\phi \hat{\mathbf{s}} + \cos\phi \hat{\boldsymbol{\phi}} \\ \hat{\mathbf{z}} = \hat{\mathbf{z}} \end{cases}$$

$$\begin{cases} s = \sqrt{x^2 + y^2} \\ \phi = \tan^{-1}(y/x) \\ z = z \end{cases} \begin{cases} \hat{\mathbf{s}} = \cos\phi \hat{\mathbf{x}} + \sin\phi \hat{\mathbf{y}} \\ \hat{\boldsymbol{\phi}} = -\sin\phi \hat{\mathbf{x}} + \cos\phi \hat{\mathbf{y}} \\ \hat{\mathbf{z}} = \hat{\mathbf{z}} \end{cases}$$

## Standaardintegralen .

m	n	I	m	n	1
-2	-1/2	$-Y/(a^2x)$	1	-3/2	-1/Y
-2	-1	$-a^{-2}(\frac{1}{x} + \frac{1}{a}\arctan\frac{x}{a})$	1	-1	ln  Y
-1	-3/2	$a^{-2}\left(\frac{1}{Y} - \frac{1}{a}\ln\left \frac{a+Y}{x}\right \right)$	1	-1/2	Y
-1	-1/2	$-(1/a)\ln\left (a+Y)/x\right $	1	1/2	$\frac{1}{3}Y^3$
-1	-1	$a^{-2} \ln  x/Y $	1	3/2	$\frac{1}{5}Y^5$
0	-3/2	$x/(a^2Y)$	2	-3/2	$\ln  x+Y  - x/Y$
0	-1	$a^{-1}\arctan(x/a)$	2	-1	$x-a\arctan(x/a)$
0	-1/2	$\ln  x+Y $	2	-1/2	$\frac{1}{2}xY - \frac{1}{2}a^2 \ln  x+Y $
0	1/2	$\frac{1}{2}xY + \frac{1}{2}a^2 \ln  x+Y $	2	1/2	$\frac{1}{8}x(2x^2+a^2)Y-\frac{1}{8}a^4\ln x+Y $
0	3/2	$\frac{1}{8}x(2x^2+5a^2)Y+\frac{3}{8}a^4\ln x+Y $	3	-3/2	$Y+a^2/Y$
			3	-1/2	$\frac{1}{3}Y^3 - a^2Y$
			3	1/2	$\frac{1}{5}Y^5 - \frac{1}{3}a^2Y^3$

m	n	I	m	n	1
1	0	$-(1/a)\cos ax$	1	1	$(\sin^2 ax)/2a$ of $-(\cos^2 ax)/2a$
0	1	$(1/a)\sin ax$	2	2	$-\frac{1}{32a}\sin 4ax + \frac{x}{8}$
1	-1	$-(1/a)\ln\left \cos ax\right $	ı	n	$-\frac{\cos^{n+1}ax}{(n+1)a}$
-1	1	$(1/a) \ln \left  \sin ax \right $	m	1	$\frac{\sin^{m+1}ax}{(m+1)a}$
2	0	$\frac{1}{2}x - \frac{1}{4a}\sin 2ax$	0	2	$\frac{1}{2}x + \frac{1}{4a}\sin 2ax$
3	0	$-\frac{1}{3a}\cos ax(\sin^2 ax + 2)$	0	3	$\frac{1}{3a}\sin ax(\cos^2 ax + 2)$
4	0	$\frac{3x}{8} - \frac{\sin 2ax}{4a} + \frac{\sin 4ax}{32a}$	0	4	$\frac{3x}{8} + \frac{\sin 2ax}{4a} + \frac{\sin 4ax}{32a}$

## 6.5 Benaderingen voor $|x| \rightarrow 0$

$(1+x)^a$	1+ax+	sin x	$x-x^3/6+$	
e <sup>x</sup>	1+x+	cosx	$1-x^2/2+$	
ln(1+x)	$x-x^3/2+$			1

Cartesian.  $d\mathbf{l} = dx \,\hat{\mathbf{x}} + dy \,\hat{\mathbf{y}} + dz \,\hat{\mathbf{z}}; \quad d\tau = dx \, dy \, dz$ 

Gradient:  $\nabla t = \frac{\partial t}{\partial x} \hat{\mathbf{x}} + \frac{\partial t}{\partial y} \hat{\mathbf{y}} + \frac{\partial t}{\partial z} \hat{\mathbf{z}}$ 

Divergence:  $\nabla \cdot \mathbf{v} = \frac{\partial v_x}{\partial x} + \frac{\partial v_y}{\partial y} + \frac{\partial v_z}{\partial z}$ 

Curl:  $\nabla \times \mathbf{v} = \left(\frac{\partial v_z}{\partial y} - \frac{\partial v_y}{\partial z}\right) \hat{\mathbf{x}} + \left(\frac{\partial v_x}{\partial z} - \frac{\partial v_z}{\partial x}\right) \hat{\mathbf{y}} + \left(\frac{\partial v_y}{\partial x} - \frac{\partial v_x}{\partial y}\right) \hat{\mathbf{z}}$ 

Laplacian:  $\nabla^2 t = \frac{\partial^2 t}{\partial x^2} + \frac{\partial^2 t}{\partial y^2} + \frac{\partial^2 t}{\partial z^2}$ 

**Spherical.**  $d\mathbf{l} = dr \,\hat{\mathbf{r}} + r \, d\theta \,\hat{\boldsymbol{\theta}} + r \sin\theta \, d\phi \,\hat{\boldsymbol{\phi}}; \quad d\tau = r^2 \sin\theta \, dr \, d\theta \, d\phi$ 

Gradient:  $\nabla t = \frac{\partial t}{\partial r} \hat{\mathbf{r}} + \frac{1}{r} \frac{\partial t}{\partial \theta} \hat{\boldsymbol{\theta}} + \frac{1}{r \sin \theta} \frac{\partial t}{\partial \phi} \hat{\boldsymbol{\phi}}$ 

Divergence:  $\nabla \cdot \mathbf{v} = \frac{1}{r^2} \frac{\partial}{\partial r} (r^2 v_r) + \frac{1}{r \sin \theta} \frac{\partial}{\partial \theta} (\sin \theta v_\theta) + \frac{1}{r \sin \theta} \frac{\partial v_\phi}{\partial \phi}$ 

Curl:  $\nabla \times \mathbf{v} = \frac{1}{r \sin \theta} \left[ \frac{\partial}{\partial \theta} (\sin \theta \, v_{\phi}) - \frac{\partial v_{\theta}}{\partial \phi} \right] \hat{\mathbf{r}}$  $+ \frac{1}{r} \left[ \frac{1}{\sin \theta} \frac{\partial v_{r}}{\partial \phi} - \frac{\partial}{\partial r} (r v_{\phi}) \right] \hat{\boldsymbol{\theta}} + \frac{1}{r} \left[ \frac{\partial}{\partial r} (r v_{\theta}) - \frac{\partial v_{r}}{\partial \theta} \right] \hat{\boldsymbol{\phi}}$ 

Laplacian:  $\nabla^2 t = \frac{1}{r^2} \frac{\partial}{\partial r} \left( r^2 \frac{\partial t}{\partial r} \right) + \frac{1}{r^2 \sin \theta} \frac{\partial}{\partial \theta} \left( \sin \theta \frac{\partial t}{\partial \theta} \right) + \frac{1}{r^2 \sin^2 \theta} \frac{\partial^2 t}{\partial \phi^2}$ 

Cylindrical.  $d\mathbf{l} = ds\,\hat{\mathbf{s}} + s\,d\phi\,\hat{\boldsymbol{\phi}} + dz\,\hat{\mathbf{z}}; d\tau = s\,ds\,d\phi\,dz$ 

Gradient:  $\nabla t = \frac{\partial t}{\partial s} \hat{s} + \frac{1}{s} \frac{\partial t}{\partial \phi} \hat{\phi} + \frac{\partial t}{\partial z} \hat{z}$ 

Divergence:  $\nabla \cdot \mathbf{v} = \frac{1}{s} \frac{\partial}{\partial s} (s v_s) + \frac{1}{s} \frac{\partial v_{\phi}}{\partial \phi} + \frac{\partial v_z}{\partial z}$ 

Curl:  $\nabla \times \mathbf{v} = \left[ \frac{1}{s} \frac{\partial v_z}{\partial \phi} - \frac{\partial v_\phi}{\partial z} \right] \hat{\mathbf{s}} + \left[ \frac{\partial v_s}{\partial z} - \frac{\partial v_z}{\partial s} \right] \hat{\boldsymbol{\phi}} + \frac{1}{s} \left[ \frac{\partial}{\partial s} (s v_\phi) - \frac{\partial v_s}{\partial \phi} \right] \hat{\mathbf{z}}$ 

Laplacian:  $\nabla^2 t = \frac{1}{s} \frac{\partial}{\partial s} \left( s \frac{\partial t}{\partial s} \right) + \frac{1}{s^2} \frac{\partial^2 t}{\partial \phi^2} + \frac{\partial^2 t}{\partial z^2}$ 

**Triple Products** 

(1)  $\mathbf{A} \cdot (\mathbf{B} \times \mathbf{C}) = \mathbf{B} \cdot (\mathbf{C} \times \mathbf{A}) = \mathbf{C} \cdot (\mathbf{A} \times \mathbf{B})$ 

(2)  $\mathbf{A} \times (\mathbf{B} \times \mathbf{C}) = \mathbf{B}(\mathbf{A} \cdot \mathbf{C}) - \mathbf{C}(\mathbf{A} \cdot \mathbf{B})$ 

**Product Rules** 

(3)  $\nabla (fg) = f(\nabla g) + g(\nabla f)$ 

(4)  $\nabla (\mathbf{A} \cdot \mathbf{B}) = \mathbf{A} \times (\nabla \times \mathbf{B}) + \mathbf{B} \times (\nabla \times \mathbf{A}) + (\mathbf{A} \cdot \nabla)\mathbf{B} + (\mathbf{B} \cdot \nabla)\mathbf{A}$ 

(5)  $\nabla \cdot (f\mathbf{A}) = f(\nabla \cdot \mathbf{A}) + \mathbf{A} \cdot (\nabla f)$ 

(6)  $\nabla \cdot (\mathbf{A} \times \mathbf{B}) = \mathbf{B} \cdot (\nabla \times \mathbf{A}) - \mathbf{A} \cdot (\nabla \times \mathbf{B})$ 

(7)  $\nabla \times (f\mathbf{A}) = f(\nabla \times \mathbf{A}) - \mathbf{A} \times (\nabla f)$ 

(8)  $\nabla \times (\mathbf{A} \times \mathbf{B}) = (\mathbf{B} \cdot \nabla)\mathbf{A} - (\mathbf{A} \cdot \nabla)\mathbf{B} + \mathbf{A}(\nabla \cdot \mathbf{B}) - \mathbf{B}(\nabla \cdot \mathbf{A})$ 

**Second Derivatives** 

(9)  $\nabla \cdot (\nabla \times \mathbf{A}) = 0$ 

(10)  $\nabla \times (\nabla f) = 0$ 

(11)  $\nabla \times (\nabla \times \mathbf{A}) = \nabla (\nabla \cdot \mathbf{A}) - \nabla^2 \mathbf{A}$ 

**FUNDAMENTAL THEOREMS** 

Gradient Theorem :  $\int_{\mathbf{a}}^{\mathbf{b}} (\nabla f) \cdot d\mathbf{l} = f(\mathbf{b}) - f(\mathbf{a})$ 

Divergence Theorem :  $\int (\nabla \cdot \mathbf{A}) d\tau = \oint \mathbf{A} \cdot d\mathbf{a}$ 

Curl Theorem :  $\int (\nabla \times \mathbf{A}) \cdot d\mathbf{a} = \oint \mathbf{A} \cdot d\mathbf{I}$