

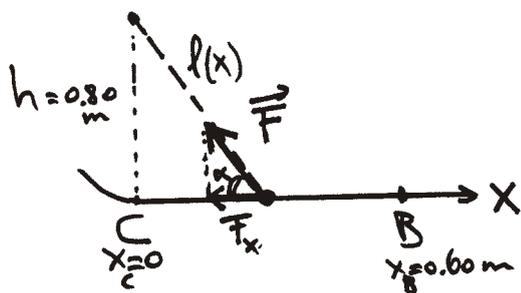
# Solutions Dynamica, Exam II, March 19, 2004

1 a. No, the spring force is always perpendicular to the direction of movement in the circular part of the rod

b. Gravity is the only force doing work:

$$\frac{1}{2}mv_c^2 = mgh \Rightarrow v_c = \sqrt{2gh} = \sqrt{2gR} = \sqrt{2 \cdot 9.81 \cdot 0.80} = 3.96 \text{ m/s}$$

c. The spring is now performing work on the slider



$$l(x) = \sqrt{h^2 + x^2}$$

$$|\vec{F}| = ku = k(l(x) - l_0)$$

↑ unstretched length

$$F_x = -|\vec{F}| \cos \alpha = -k(l - l_0) \frac{x}{l} = -kx \left(1 - \frac{l_0}{\sqrt{h^2 + x^2}}\right)$$

$$W = \int_{x_c}^{x_B} F_x dx = - \int_0^{x_B} kx dx + \int_0^{x_B} \frac{kl_0 x}{\sqrt{h^2 + x^2}} dx =$$

$$= -\frac{1}{2}kx_B^2 + \frac{1}{2}l_0 \int_0^{x_B} k(h^2 + x^2)^{-1/2} d(h^2 + x^2) = -\frac{1}{2}kx_B^2 + kl_0 \sqrt{h^2 + x^2} \Big|_0^{x_B} =$$

$$= -\frac{1}{2}kx_B^2 + kl_0(\sqrt{h^2 + x_B^2} - \sqrt{h^2}) = -20 \text{ J}$$

$$\frac{1}{2}mv_B^2 = \frac{1}{2}mv_c^2 + W \Rightarrow v_B = \sqrt{v_c^2 + \frac{2W}{m}} = 1.54 \text{ m/s}$$

d. Then,  $\frac{1}{2}mv_c^2 + W = 0 \Rightarrow$

$$2mgh - \frac{1}{2}kx^2 + kl_0(\sqrt{x^2 + h^2} - h) = 0$$

define:  $u = \sqrt{x^2 + h^2} \Rightarrow u^2 - 2l_0u + C = 0$   
with  $C = 2l_0h - h^2 - \frac{4mgh}{k} \approx$

solution:  $u = l_0(1 + \sqrt{1 - C/l_0^2}) \Rightarrow u = 1.19 \text{ m}$

$$\sqrt{x^2 + h^2} = l_0(1 + \sqrt{1 - C/l_0^2}) \Rightarrow \sqrt{x^2 + h^2} = 1.19 \text{ m}$$

$$x = \sqrt{1.19^2 - 0.8^2} = 0.89 \text{ m}$$

2 a. The energy of the compressed spring is converted into kinetic energy of the pea:

$$\frac{1}{2} k \Delta X^2 = \frac{1}{2} m v^2 \Rightarrow v = \sqrt{\frac{k}{m}} \Delta X \quad (1)$$

The time it takes the pea to fall to the ground is independent of its horizontal velocity; therefore:  $s = vt$  or:  
 $s \sim v$  (2)

$$\text{Now: } \frac{s_2}{s_1} = \frac{v_2}{v_1} = \frac{\Delta X_2}{\Delta X_1} \Rightarrow \Delta X_2 = \frac{s_2}{s_1} \Delta X_1 = 0.80 \cdot 2.00 \text{ m} = 1.6 \text{ cm}$$

b. If  $\Delta X_2 = \Delta X_1$ , then  $v_2 = v_1$ .

$$\frac{s_2}{s_1} = \frac{v_2 t_2}{v_1 t_1} = \frac{t_2}{t_1}$$

Since  $h = \frac{1}{2} g t^2$  we have  $t = \sqrt{\frac{2h}{g}}$ , so (3)

$$\frac{t_2}{t_1} = \frac{\sqrt{\frac{2h_2}{g}}}{\sqrt{\frac{2h_1}{g}}} = \sqrt{\frac{h_2}{h_1}} \Rightarrow \frac{h_2}{h_1} = \left(\frac{t_2}{t_1}\right)^2 = \left(\frac{s_2}{s_1}\right)^2 = (0.80)^2 = 0.64$$

$$\Rightarrow h_2 = 0.64 \cdot 0.8 \text{ m} = 0.512 \text{ m}$$

$$\text{c. } k = \frac{4.0 \text{ N}}{2.0 \cdot 10^{-2} \text{ m}} = 200 \text{ N/m}$$

Combining (1), (2), and (3) we have:

$$s_1 = v_1 \cdot t_1 = \left(\sqrt{\frac{k}{m}} \Delta X_1\right) \left(\sqrt{\frac{2h_1}{g}}\right) = \sqrt{\frac{2kh_1}{mg}} \Delta X_1 \Rightarrow$$

$$m = \frac{\Delta X_1^2}{s_1^2} \cdot \frac{2kh_1}{g} = \frac{0.020^2}{2.5^2} \cdot \frac{2 \cdot 200 \cdot 0.8}{9.81} =$$

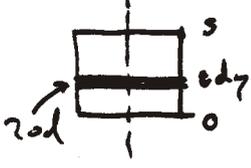
$$= 2.1 \cdot 10^{-3} \text{ kg} = 2.1 \text{ g}$$

3. a.

A thin rod of mass  $m_2$  and length  $L$  has rotational inertia  $I_2 = \frac{1}{12} m_2 L^2$  with respect to the symmetry axis perpendicular to the rod (see book). The rotational inertia of a square slab of mass  $M$  and size  $S$  can be calculated from the above:

$$I_S = \int_0^S dI_{rod} = \int_0^S \frac{1}{12} (dm) S^2 = \frac{1}{12} M S^3 \int_0^S dy =$$

$\uparrow$  mass per  $m^2$

$$= \frac{1}{12} M S^4 = \frac{1}{12} M S^2 \Rightarrow$$


$$I_{largeslab} = \frac{1}{12} m_s \cdot (2a)^2 = \frac{1}{3} m_s a^2$$

$$I_{smallslab} = \frac{1}{12} \cdot \left(\frac{1}{4} m_s\right) \cdot a^2 = \frac{1}{48} m_s a^2$$

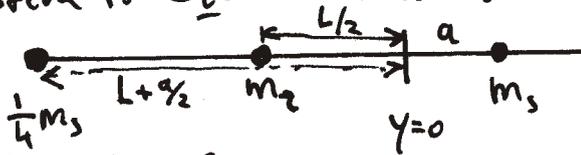
With the parallel axis theorem, we now can calculate  $I$ :

$$I = I_2 + m_2 \left(\frac{1}{2} L\right)^2 + I_{largeslab} + m_s \cdot a^2$$

$$+ I_{smallslab} + \left(\frac{1}{4} m_s\right) \left(L + \frac{1}{2} a\right)^2 =$$

$$= \frac{1}{3} m_2 L^2 + \frac{17}{12} m_s a^2 + \frac{1}{4} m_s L \left(L + \frac{1}{2} a\right)$$

b. The system is equivalent with:



which has the COM:

$$y_{com} = a m_s - \frac{L}{2} m_2 - \left(L + \frac{a}{2}\right) \cdot \left(\frac{1}{4} m_s\right) =$$

$$= \left(\frac{7}{8} a - \frac{1}{4} L\right) m_s - \frac{L}{2} m_2$$

$$y_{com} = 0 \Rightarrow m_2 = \left(\frac{7}{4} \frac{a}{L} - \frac{1}{2}\right) m_s$$

$$= \frac{3}{8} m_s = 0.9 \text{ kg}$$

3. c. The total angular momentum before and after this (completely inelastic) collision must be equal:

$$I\omega + L_{\text{bird}} = I'\omega'$$

Here  $I' = I + m_b R^2$  is the rotational inertia of bird and vane combined, and  $\omega'$  is the angular velocity after the collision.

$$|L_{\text{bird}}| = m_b |\vec{r}_b \times \vec{v}_b| = m_b R V, \quad \text{so:}$$

$$\begin{aligned} \omega' &= \frac{I\omega + m_b R V}{I'} = \frac{1.216 \cdot 1.0 + 0.4 \cdot 0.60 \cdot 1.2}{(1.216 + 0.4 \cdot 0.60^2)} \\ &= 1.11 \text{ rad/s} \end{aligned}$$

The kinetic energy increase of the wind vane is now:

$$\Delta E = \frac{1}{2} I \omega'^2 - \frac{1}{2} I \omega^2 = \frac{1}{2} \cdot 1.216 (1.11^2 - 1.0^2) = 0.136 \text{ J}$$

- d. Angular momentum conservation:

$$I\omega - m_b a V = I\omega' - m_b a V' \Rightarrow$$

$$I(\omega' - \omega) = -m_b a (V - V') \quad (1)$$

kin. energy conservation:

$$\frac{1}{2} I \omega^2 + \frac{1}{2} m_b V^2 = \frac{1}{2} I \omega'^2 + \frac{1}{2} m_b V'^2 \Rightarrow$$

$$I(\omega'^2 - \omega^2) = m_b (V^2 - V'^2)$$

$$I(\omega' - \omega)(\omega' + \omega) = m_b (V - V')(V + V') \Rightarrow (1)$$

$$-m_b a (V - V')(\omega' + \omega) = m_b (V - V')(V + V')$$

$$-a(\omega' + \omega) = V + V' \quad (2)$$

(1) + (-m\_b a) (2) gives:

$$\omega' = \frac{(I - m_b a^2)\omega - 2m_b a V}{I + m_b a^2} =$$

$$= \frac{(1.216 - 0.064) \cdot 1.0 - 2 \cdot 0.4 \cdot 0.4 \cdot 1.2}{1.216 + 0.064} = 0.6 \text{ rad/s.}$$

kinetic energy loss:

$$\Delta E = \frac{1}{2} I \omega'^2 - \frac{1}{2} I \omega^2 = \frac{1}{2} \cdot 1.216 (0.6^2 - 1.0^2) = -0.384 \text{ J.}$$

4.a. Rotational inertia of cylinder of length  $L$  and radius  $R$  around its vertical symmetry axis:

$$I = \int_{\phi=0}^{2\pi} \int_{z=0}^L \int_{r=0}^R \rho r^2 r dr d\phi dz = 2\pi \rho L \cdot \frac{1}{4} R^4 = \frac{1}{2} \pi \rho L R^4$$

where  $\rho$  is the density. For the dumbbell:

$$I_{\text{tot}} = \frac{1}{2} \pi \rho l R_1^4 + 2 \cdot \frac{1}{2} \pi \rho \left(\frac{1}{2}l\right) R_2^4 =$$

$$= \frac{1}{2} \pi \rho l (R_1^4 + R_2^4)$$

$$M = \rho \cdot \left( \pi R_1^2 l + 2 \cdot \pi R_2^2 \left(\frac{1}{2}l\right) \right) = \rho \pi l (R_1^2 + R_2^2) \Rightarrow$$

$$I_{\text{tot}} = \frac{1}{2} M \frac{R_1^4 + R_2^4}{R_1^2 + R_2^2}$$

b. around A: angular acceleration

$$I_{\text{tot}} \alpha_{\text{cm}} = \tau$$

$$\tau = |\vec{\tau}| = |\vec{r} \times \vec{F}_z| = Mg R_1 \sin \alpha$$

$$I_{\text{tot}} \alpha_{\text{cm}} = I_{\text{tot}} + MR_1^2 = \frac{1}{2} M \frac{R_1^4 + R_2^4}{R_1^2 + R_2^2} + MR_1^2 = \frac{1}{2} M \frac{3R_1^4 + 2R_1^2 R_2^2 + R_2^4}{R_1^2 + R_2^2}$$

(parallel axis theorem)

$$\alpha_{\text{cm}} = R_1 \alpha_{\text{cm}} = \frac{Mg R_1 \sin \alpha}{I_{\text{tot}}} = \frac{2g \sin \alpha}{\frac{3R_1^4 + 2R_1^2 R_2^2 + R_2^4}{R_1^2 + R_2^2}} = 0.0_{\dots} 658 g = 0.65 \text{ m/s}^2$$

c. Around central axis: (same col. acceleration!)

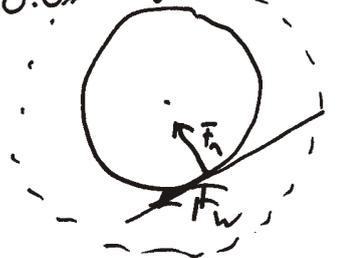
$$I_{\text{tot}} \alpha_{\text{cm}} = F_w R_1 \Rightarrow F_w = \frac{I_{\text{tot}} \alpha_{\text{cm}}}{R_1^2} =$$

$$= \frac{1}{2} M \frac{R_1^4 + R_2^4}{R_1^2 + R_2^2} \cdot \frac{2g \sin \alpha}{\frac{3R_1^4 + 2R_1^2 R_2^2 + R_2^4}{R_1^2 + R_2^2}} =$$

$$= Mg \sin \alpha \frac{R_1^4 + R_2^4}{3R_1^4 + 2R_1^2 R_2^2 + R_2^4} \quad F_n = Mg \cos \alpha \quad F_w = \mu F_n \Rightarrow$$

$$\mu_{\text{min}} = \frac{F_w}{F_n} = \tan \alpha \frac{R_1^4 + R_2^4}{3R_1^4 + 2R_1^2 R_2^2 + R_2^4} = 0.50$$

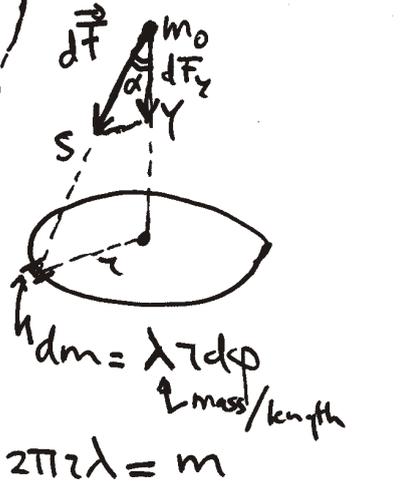
d.  $s = \frac{1}{2} a_{\text{cm}} t^2 \Rightarrow t = \sqrt{\frac{2s}{a_{\text{cm}}}} = \sqrt{\frac{1.0}{0.65}} = 1.24 \text{ s.}$



5. a.  $|\vec{dF}| = G m_0 \frac{dm}{s^2}$  ;  $|d\vec{F}_y| = |\vec{dF}| \cos \alpha = \frac{d\vec{F}_y}{s}$

$$|\vec{F}| = \int_{\varphi=0}^{2\pi} |d\vec{F}_y| = \frac{G m_0 \lambda y z}{(\sqrt{y^2+z^2})^{3/2}} \int_0^{2\pi} d\varphi =$$

$$= \frac{G m_0 \gamma (\lambda 2\pi z)}{(y^2+z^2)^{3/2}} = \frac{G m m_0 \gamma}{(y^2+z^2)^{3/2}}$$



b.  $\frac{1}{2} m_0 v^2 = - \int_{y=y_0}^0 |\vec{F}| dy = \int_0^{y_0} \frac{G m m_0 \gamma dy}{(y^2+z^2)^{3/2}} =$

$$= \frac{1}{2} G m m_0 \int_0^{y_0} (y^2+z^2)^{-3/2} d(y^2+z^2)$$

$$= \frac{1}{2} G m m_0 \left[ -2 (y^2+z^2)^{-1/2} \right]_0^{y_0} =$$

$$= G m m_0 \left( \frac{1}{z} - \frac{1}{\sqrt{y_0^2+z^2}} \right) \Rightarrow$$

$$v = \sqrt{2 G m \left( \frac{1}{z} - \frac{1}{\sqrt{z^2+y_0^2}} \right)} \quad (\cdot v = v(0))$$

c.  $v = \sqrt{\frac{2 G m}{z} \left( 1 - \frac{1}{\sqrt{1 + \left(\frac{y_0}{z}\right)^2}} \right)} \approx \sqrt{\frac{2 G m}{z}} \sqrt{1 - \frac{1}{1 + \frac{1}{2} \left(\frac{y_0}{z}\right)^2}}$

$$\approx \sqrt{\frac{2 G m}{z}} \sqrt{1 - \left( 1 - \frac{1}{2} \left(\frac{y_0}{z}\right)^2 + \mathcal{O}\left(\frac{y_0}{z}\right)^4 \right)} =$$

$$= \sqrt{\frac{2 G m}{z}} \sqrt{\frac{1}{2} \left(\frac{y_0}{z}\right)^2 + \mathcal{O}\left(\frac{y_0}{z}\right)^4} = \sqrt{G m} \frac{y_0}{z^{3/2}} + \mathcal{O}\left(\frac{y_0}{z}\right)^2$$

d. for  $\frac{y_0}{z} \ll 1$  we can also do a Taylor-expansion of the force acting on  $m_0$ :

$$F = \frac{G m m_0 \gamma}{z^3 \left( 1 + \frac{y_0^2}{z^2} \right)^{3/2}} \approx \frac{G m m_0 \gamma}{z^2} \cdot \frac{y_0}{z} \cdot \left( 1 - \frac{3}{2} \frac{y_0^2}{z^2} \right) \approx$$

$$\approx \frac{G m m_0 \gamma}{z^3} y \quad \text{in leading order.}$$

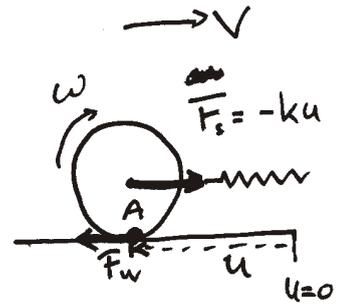
Note that the force is directed towards  $y=0$  always, such that

$$m_0 \ddot{y} = - \frac{G m m_0 \gamma}{z^3} y \Rightarrow \ddot{y} + \frac{G m}{z^3} y = 0$$

This is a harmonic oscillator with frequency:

$$\omega = \sqrt{\frac{G m}{z^3}} \Rightarrow f = \frac{\omega}{2\pi} = \frac{1}{2\pi} \sqrt{\frac{G m}{z^3}}$$

6. At the release position, the system only has potential energy:  $\frac{1}{2}k u_{\max}^2$   
 As it passes through the equilibrium position it has only kinetic energy, both translational and rotational:  $\frac{1}{2}I\omega^2 + \frac{1}{2}MV^2$



Now:  $I = \frac{1}{2}MR^2$  (see book)

$V = \omega R$  (no slipping), so energy balance gives:

$$\frac{1}{2}k u_{\max}^2 = \frac{1}{2}I\omega^2 + \frac{1}{2}MV^2 = \left(\frac{1}{2}\frac{I}{R^2} + \frac{1}{2}M\right)V^2 = \frac{1}{2}\left(\frac{1}{2}M + M\right)V^2 \Rightarrow$$

$$V = \sqrt{\frac{2k}{3M}} u_{\max} \quad \text{is the velocity at the equilibrium position}$$

- a. Translational kinetic energy at equilibrium position:

$$K_{\text{trans}} = \frac{1}{2}MV^2 = \frac{1}{2}M \frac{2k}{3M} u_{\max}^2 = \frac{1}{3}k u_{\max}^2 = 7.5 \text{ J}$$

- b. Rotational kinetic energy at equilibrium position:

$$K_{\text{rot}} = \frac{1}{2}I\omega^2 = \frac{1}{2}\frac{I}{R^2}V^2 = \frac{1}{4}M \frac{2k}{3M} u_{\max}^2 = \frac{1}{6}k u_{\max}^2 = 3.75 \text{ J}$$

(Note that  $T_{\text{trans}} + T_{\text{rot}} = \frac{1}{2}k u_{\max}^2$ , as it should be.)

- c. Since  $F_w$  is unknown, calculate the rotational acceleration around point A:

$$I' \alpha = F_s R$$

$$\ddot{u} = a = \alpha R \quad (\text{rolling without slipping})$$

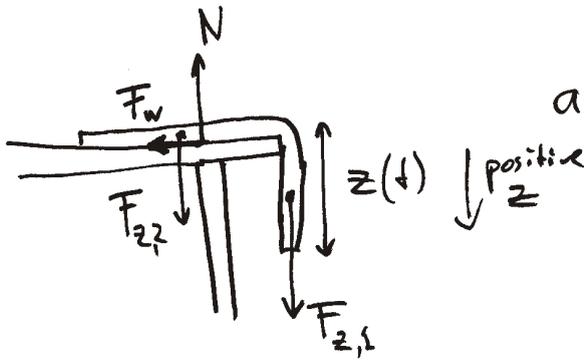
$$I' = I + MR^2 = \frac{3}{2}MR^2 \quad (\text{parallel axis theorem})$$

$$\frac{3}{2}MR^2 \cdot \frac{\ddot{u}}{R} = -ku R \Rightarrow \frac{3}{2}M\ddot{u} = -ku \Rightarrow$$

$$\ddot{u} + \frac{2k}{3M}u = 0 \quad \text{harmonic oscillator with } \omega^2 = \frac{2k}{3M}$$

$$\text{so: } T = \frac{2\pi}{\omega} = \frac{2\pi}{\sqrt{\frac{2k}{3M}}} = 2\pi \sqrt{\frac{3M}{2k}}$$

7.



$$\begin{aligned} \text{a. } F_{z,1} &= \frac{z}{L} Mg \\ F_{z,2} &= \frac{L-z}{L} Mg = N \\ F_w &= \mu N = \mu \frac{L-z}{L} Mg \end{aligned}$$

$$\begin{aligned} M\ddot{z} &= \sum F = F_{z,1} - F_w = \frac{z}{L} Mg - \mu \frac{L-z}{L} Mg = \\ &= (1+\mu) \frac{Mg}{L} z - \mu Mg \Rightarrow \\ \ddot{z} - (1+\mu) \frac{g}{L} z + \mu g &= 0 \quad (1) \end{aligned}$$

b. We show that (1) is solved by inserting the function and finding  $\omega$ ,  $C$ ,  $A$  and  $B$  that solve the problem:

$$\begin{aligned} z(t) &= Ae^{\omega t} + Be^{-\omega t} + C \Rightarrow \\ \dot{z}(t) &= \omega Ae^{\omega t} - \omega Be^{-\omega t} \Rightarrow \\ \ddot{z}(t) &= \omega^2 Ae^{\omega t} + \omega^2 Be^{-\omega t} = \omega^2(z(t) - C) \end{aligned}$$

Inserting in (1):

$$\omega^2(z(t) - C) - (1+\mu) \frac{g}{L} z(t) + \mu g = 0 \Rightarrow$$

$$\left(\omega^2 - (1+\mu) \frac{g}{L}\right) z(t) + \mu g - \omega^2 C = 0 \quad \text{This holds for all } t \text{ if:}$$

$$\omega = \sqrt{(1+\mu) \frac{g}{L}} \quad \text{and} \quad C = \frac{\mu g}{\omega^2} = \frac{\mu g}{(1+\mu) \frac{g}{L}} = \frac{\mu L}{1+\mu}$$

From the initial conditions,  $z(0) = L/3$ ,  $\dot{z}(0) = 0$ , we determine  $A$  and  $B$ :

$$\dot{z}(0) = 0 \Rightarrow \omega A - \omega B = 0 \Rightarrow A = B$$

$$z(0) = L/3 \Rightarrow A + B + C = L/3 \Rightarrow 2A + \frac{\mu L}{1+\mu} = \frac{L}{3} \Rightarrow$$

$$A = \frac{L}{6} \frac{(1-2\mu)}{1+\mu}$$

$$\text{So: } z(t) = \frac{L}{6} \frac{(1-2\mu)}{1+\mu} (e^{\omega t} + e^{-\omega t}) + L \left( \frac{\mu}{1+\mu} \right)$$

$$\begin{aligned} \omega &= \sqrt{(1+\mu) \frac{g}{L}} \\ &= \frac{1}{2}(e^{\omega t} + e^{-\omega t}) = \cosh(\omega t) \end{aligned}$$

$$= \frac{L}{3} \frac{(1-2\mu)}{1+\mu} \cosh\left(\sqrt{(1+\mu) \frac{g}{L}} t\right) + L \left( \frac{\mu}{1+\mu} \right)$$